

# HIGH THROUGHPUT HIGH-YIELD VACUUM DEPOSITION SYSTEM FOR THIN FILM BASED DENSE WAVELENGTH DIVISION MULTIPLEXERS

## 5 I. Background Of The Invention

### A. Field Of The Invention

10 This application claims priority to U.S. Provisional Patent Application Serial No. 60/217, 060, entitled HIGH THROUGHPUT HIGH-YIELD VACUUM DEPOSITION SYSTEM FOR THIN FILM BASED DENSE WAVELENGTH DIVISION MULTIPLEXERS, filed on July 10, 2000 and U.S. Provisional Patent Application Serial No. 60/217,115, entitled SUBSTRATE FIXTURE FOR HIGH-YIELD PRODUCTION OF THIN FILM BASED DENSE WAVELENGTH DIVISION MULTIPLEXERS, filed  
15 on July 10, 2000.

20 The present invention relates to the installation of a worldwide fiber-optic network, which is in progress, capable of handling levels of data transmission inconceivable only several years ago. As a result of this network, the Internet is less than half a decade away from being a more useful tool than the computers which navigate it. Advanced thin film coatings have emerged as the enabling technology to control transmission and reflection of selected wavelengths of light. From this, and other technical achievements, existing optical fibers will accommodate the increase in bandwidth that is required over the next 3-5 years.

25 Dense Wavelength Division Multiplexer (DWDM) systems enable information to be delivered inside fiber-optic cables at multiple wavelengths. The increase in the bandwidth is limited only by the number of wavelengths which can be superimposed on the fiber. Current state-of-the-art DWDM can multiplex/demultiplex approximately 40  
30 channels. Ultimately more than 1000 channels will be possible. During transmission, information is packaged within pulse modulated carriers at specific wavelengths and

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superimposed (multiplexing) on the fiber. During reception, the carriers must be separated (demultiplexing). Optical component technology such as DWDM is critical in order to achieve the bandwidth necessary for future interactive services, such as "video on demand," and has prompted multi-billion dollar strategic acquisitions such as OCLI®,  
5 NetOptix™, and XROS™.

The most widely used technology for demultiplexing in DWDM systems is thin film-based. Multilayered, thin dielectric coatings are comprised of 150-200 layers with individual optical layer thickness equal to multiples of  $\frac{1}{4}$  of the wavelength to be  
10 transmitted (known as dielectric interference filters.) A collection of such filters, coupled together, each differing slightly in design to allow light transmission of different wavelengths, and "connected" to a fiber-optic cable, enables the multiplexing (superposition) and demultiplexing (separation) of multiple wavelengths of laser light containing digital information.

15 Current thin film demultiplexer filters are produced with accepted yields of less than 5%, due to the complexity and uniformity requirements of the filter designs. Coating equipment used for complex optical coatings are not optimally tooled to provide necessary uniformity for this application, and are therefore unable to produce a high  
20 throughput of certified filters. A large-area, ion assisted, electron-beam evaporation system has been designed which utilizes a novel fixture assembly resulting in a substantial improvement in yields. The system employs several modifications to conventional deposition configurations and processes to enable high throughput of narrow band pass filters for multiplexers (muxes) and demultiplexers (demuxes) in  
25 DWDM systems.

#### *B. Description Of The Related Art*

Thin film coatings designed to permit light transmission/reflection over narrow (0.1 – 25 nm) and broad (> 25 nm) band passes are typically comprised of multiple layers of two or more optically matched “high” index and “low” index materials. The individual layer thickness and number of layers will ultimately define the optical performance of the filter. Typical “high performance” narrow band filters may have more than 100 individual layers.

High performance dielectric thin film optical filters are produced in volume for state-of-the-art muxes and demuxes used in DWDM systems. These filters are produced with materials such as  $\text{SiO}_2$  and  $\text{Ta}_2\text{O}_5$  deposited with processes such as ion beam sputter deposition (ISBD) and ion-assisted deposition (IAD). Filters produced with these processes are stable under adverse environmental conditions.

Thickness uniformity is critical in any optical filter application. Optical coating systems are typically designed to produce coatings with thickness uniformity of approximately 0.1% variation over the substrate area. This level of thickness control is insufficient for multilayered coatings designed for DWDM. Layer thickness determines wavelength and amplitude (loss) of transmitted light, therefore, accurate thickness determination and reproducibility are crucial.

In practice, tens of substrates (approximately 6” square) are coated with multilayer filters designed for DWDM in “traditional” IBSD or IAD systems. A typical IAD production coating system can be approximated by a 60” cube with a fixture assembly located at the top of the vacuum chamber as shown schematically in FIGURE 1. The planetary fixture assembly is designed for thickness uniformity described above and can accommodate approximately sixteen (16) to twenty-four (24) 6” square or round substrates. As many as five QCMs (quartz crystal monitors) and an optical monitor are positioned about the chamber to monitor deposition rate and optical layer thickness. The quartz monitors are calibrated prior to production. Deposition rate incident on the

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substrate assembly is determined by sampling each monitor and averaging.

Two or three electron guns are employed to reduce the deposition time as shown in FIGURE 1A. The filter is comprised of more than 150 alternating layers, and the source material must be preheated before each layer is deposited. The preheating process can take from 30 – 120 seconds (0.5 - 2.0 minutes) which would add up to  $(0.5 - 2.0) \times 150 = 75 - 300$  additional minutes to the deposition cycle if a single gun was used.

The substrates are diced into thousands of ~ 1 mm squares (called dies or chips). Every coated die is tested for performance to determine which ones, if any, meet requirements. Major manufacturers such as OCLI® have reported production yields of less than 5%. The demand for such filters is approaching 1 million per month. This demand will not be met with the current system configurations without a significant increase in capital equipment to increase capacity. Customers for the filters have relaxed requirements and settled for inadequate performance to continue with installation of DWDM systems

A patent pending high yield fixture, called the Vornado™, has been designed to produce demux filters for DWDM systems with greater than 25% accepted yield. The design is comprised of a disk (approximately 8.5" in diameter) with a concentric multi crystal QCM and a dedicated "clam" shutter arrangement. The disk rotates at greater than 1000 rpm during operation to insure uniform deposition of material at typical coating deposition rates of 0.2 – 0.5 nm/s. The Vornado™ is capable of yielding approximately 1000 filters per deposition.

## **II. Summary Of The Invention**

A high-yield high-throughput vacuum deposition system has been designed for

production of narrow band pass filters for use in mux and demux devices of DWDM systems. The filter production system utilizes a high-yield fixture assembly call the Vornado™ and a novel moving electron gun assembly which allows symmetry between the substrates and deposition source to be maintained. With proper system calibration, and modifications to conventional vacuum deposition processes used to produce filters for DWDM components, the system is capable of yields greater than 25% and a production capacity of greater than 15,000 filters per deposition.

In accordance with one aspect of the present invention, an ion-assisted electron beam evaporation process includes the steps of positioning multiple high yield fixtures in an array, adjusting a vertical position of each of the fixtures to compensate for variations in deposition rate versus chamber location, providing two electron guns, mounting the guns to a movable track, positioning the first gun at a source deposition location, rotating the fixture at greater than 2400 revolutions per minute, performing ion assisted evaporation with the first gun, the second gun being kept in a stand-by location in pre-heat mode, ceasing deposition prior to achieving target thickness, shuttering each of the fixtures at different times, independently reopening the fixtures to a low rate pulsed deposition to achieve the target thickness, closing clam shutters on the fixtures, moving the first gun to a stand-by position, moving the second gun to the source deposition location, sampling evaporation with a quartz crystal thickness monitor, opening a shutter on the second gun, performing ion assisted evaporation with the second gun, the first gun being kept in a stand-by location in pre-heat mode, ceasing deposition prior to achieving target thickness, shuttering each of the fixtures at different times, independently reopening the fixtures to a low rate pulsed deposition to achieve the target thickness, closing clam shutters on the fixtures, and repeating the process until desired filter is obtained.

In accordance with another aspect of the present invention, a method for producing an optical filter utilizing line-of-sight deposition includes the steps of

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providing multiple substrates, providing a fixed ion source, providing at least one selectively movable evaporator, positioning the at least one evaporator at a source deposition location, and depositing material onto the substrates.

5           In accordance with still another aspect of the present invention, the method includes shuttering the substrates as necessary to ensure uniform deposition on the substrates.

10           In accordance with yet another aspect of the present invention, the method includes ceasing deposition of a layer prior to achieving target thickness, shuttering the substrates at different times, independently unshuttering the substrates, and achieving the target thickness.

15           In accordance with another aspect of the present invention, the method includes moving the first evaporator to a stand-by position, opening a shutter on the second evaporator, positioning the second evaporator at the source deposition location, performing ion assisted evaporation with the second evaporator, ceasing deposition of a layer prior to achieving target thickness, shuttering the substrates at different times, independently unshuttering the substrates, and achieving the target thickness.

20           In accordance with yet another aspect of the present invention, after moving the second evaporator into the source deposition location, the method includes sampling evaporation with a quartz crystal thickness monitor.

25           In accordance with still another aspect of the present invention, the method further includes the steps of closing clam shutters on the substrates, repeating the process until desired filter is obtained, and providing a dense high yield fixture array having multiple, independently shutterable fixtures, each of the fixtures containing multiple substrates.

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In accordance with another aspect of the present invention, a system for producing optical filters includes multiple substrates, an ion source, at least two selectively movable evaporators, a source deposition location, shuttering means for shuttering the substrates, and a vacuum chamber.

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In accordance with yet another aspect of the present invention, the substrates are attached to high yield fixtures, the fixtures being independently shutterable, the fixtures rotate and are adjustable, the evaporators are connected to a movable track, the movable track being opposite the fixtures in the vacuum chamber, and the vacuum chamber is approximately 60 inches wide by 60 inches deep by 80 inches high.

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In accordance with another aspect of the present invention, the system includes a quartz crystal thickness monitor.

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Still other benefits and advantages of the invention will become apparent to those skilled in the art upon a reading and understanding of the following detailed specification.

### **III. Brief Description Of The Drawings**

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The invention may take physical form in certain parts and arrangement of parts. At least one embodiment of these parts will be described in detail in the specification and illustrated in the accompanying drawings, which form a part of this disclosure and wherein:

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FIGURE 1A shows a prior art box-style IAD coater;

FIGURE 1B shows a prior art planetary substrate assembly;

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FIGURE 2A shows the inventive deposition system with dual moveable e-beam

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evaporators; and,

FIGURE 2B shows the inventive dense high yield fixture array.

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#### **IV. Description Of The Invention**

Referring now to the drawings, which are for purposes of illustrating at least one embodiment of the invention only, and not for purposes of limiting the invention,

10 FIGURES 2A and 2 B show the invention as described with reference to at least one embodiment.

FIGURE 2A and 2B show the inventive assembly, including evaporators 10, a source deposition location 12, a standby position 14, a fixed ion source 16, a vacuum  
15 chamber 18, fixed array 20, fixtures 22, substrate 26, disk 28, rotation mechanism 30, and QCM 32. The fixtures 22 are located in a dense high yield array 20, as shown in FIGURES 2A and 2B. The fixtures 22 are in close proximity to each other, in order to utilize as many substrates 26 as possible.

20 An ion assisted electron beam evaporation system has been configured to produce narrow band pass filters for DWDM multiplexers with high throughput and maximum yield. The system significantly improves uniformity of coated substrates to enable increased output. The improvements to the conventional electron beam deposition system discussed herein can be implemented in any deposition system designed to  
25 produce high performance filters for DWDM.

The deposition system is shown schematically in FIGURE 2A. With a dense array 20 of such fixtures 22, sufficient thickness uniformity is guaranteed on substrates 26 at every location in the deposition system. In this embodiment, it is preferable that the  
30 electron beam gun 10 remain near a central location, since the dense fixture array 20 does

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not rotate in a planetary fashion. The optimum location for maximum deposition uniformity must be selected for the position of the electron gun 10. This position is called the source deposition location 12.

5           As described earlier, for highest throughput, two electron guns 10 are preferred for a two material design. If the filter design incorporated more than 2 materials, it would be desirable to employ one electron gun 10 for every material used to produce the filter. However, it is to be understood that this invention will work with any number of guns 10, as long as chosen using sound engineering judgment.

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As shown in FIGURE 2A, the electron guns 10 are mounted to a movable track 36, which allows positioning of the operational gun 10 at the source deposition location 12. In this embodiment, the gun 10 performing deposition of an individual layer is positioned at the source deposition location 12 before evaporation from that gun 10 is initiated. During alternate layers, the gun 10 not in use is kept in a stand-by location 14 and in "pre-heat" mode. As a layer deposition is concluded, the gun 10 in stand-by 14 is quickly moved from the stand-by position 14 to the source deposition location 12 and the next layer is initiated. Translation from the stand-by location 14 to the source deposition location 12 can be performed in less than 2 seconds.

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If the electron guns 10 operated flawlessly, then the source deposition location 12 would be the exact center of the chamber base plate (shown but not referenced). It is possible, in this embodiment, that the source deposition location 12 may be off-center. The moving track 36 allows the operator to determine the source deposition location 12 experimentally for each gun 10.

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The deposition process would proceed in the following way. Fixtures 22 are positioned approximately as shown in FIGURES 2A and 2B. During system calibration, the vertical position of each fixture 22 is individually adjusted to compensate for

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variations in deposition rate vs. chamber location. In FIGURE 2A, the array 20 is shown with the fixtures 22 having differing vertical positions.

Ion assisted evaporation is produced in the traditional fashion with the gun 10, containing the required layer material, positioned in the source deposition location 12. In this embodiment, the fixtures 22 rotate at approximately 1000 rpm or greater. However, it is to be understood that the fixtures can rotate as low as approximately 500 rpm as well. As the thickness of the individual layer approaches the target value as measured by the QCM 32, the clam shutter 38 closes prior to achieving the target thickness. Individual fixtures 22 are shuttered at different times, since like thicknesses are not achieved simultaneously, due to geometrical factors and nonuniform variations in deposition rate at different locations in the chamber 18.

Each fixture 22 is independently reopened to a low rate pulsed deposition process to achieve the target thickness. The low rate pulsed process utilizes a pulsed electron gun 10 while leaving the ion source 16 in full operating mode. The result is a uniform average deposition rate of approximately 0.025 mn/s and allows the layer thickness to be achieved on each fixture 22 independently. This process may take as much time as the initial "bulk" portion of the layer.

After completion of the layer all clam shutters 38 close and the electron gun 10 in the source deposition location 12 is shuttered and moves to the stand-by position 14. Simultaneously, the alternate gun 10 moves to the source deposition location 12 and the gun shutter (not shown) is opened. Each electron gun 10 uses a shuttered QCM (not shown) to sample evaporation before the clam shutters 38 are opened. The process is repeated until the desired filter is obtained. Total deposition time can range from 24-36 hours.

Obviously, modifications and alterations will occur to others upon a reading and

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understanding of the specification. It is intended by applicant to include all such modifications and alterations insofar as they come within the scope of the appended, claims or the equivalents thereof.

5           Having thus described the invention, it is now claimed:

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